

Outline

- General comments on SC cavity design choices for accelerators
- Basics of SRF cavities
 - Structure Types
- Basic RF Cavity Design Principles
- Figures of Merit
 - Gradient, Losses, Q, Shunt Impedance, Peak Fields...
- Miracle of Superconductivity
- SC/NC comparison for CW application
- Design Aspects for Multicells
- Mechanical Aspects of Cavity Design
- Cavity Performance Aspects/Cavity Technology
 - Multipacting, Breakdown (Quench), Field Emission, Q-Slope
- Ultimate gradient possibilities
- Fundamental critical fields
- Wide Range of Applications



Overall Approach

- General introduction to many workshop topics
 - Focus on high velocity structures
 - Separate tutorials on high β and low β cavity design aspects
- Important Topics not covered
 - Input couplers
 - HOM couplers
 - Tuners, Vibrations, Microphonics
 - Cryomodules



RF Cavities: Energy for Accelerators

Apply concepts to two examples: Storage Ring, Linear Collider





General Accelerator Requirements That Drive SC Cavity Design Choices

Voltage

Storage Rings

CESR-III: 7 MV, KEK-B HER: 14 MV, LEP-II: 3 GV Proton Linac: 1 GV SNS, ESS Linac-Based FEL or ERL : 500 MeV - 5 GeV

Linear Collider: 500 - 1000 GV

Duty Factor (RF on time x Repetition Rate)

Storage Rings: CW

Linac-Based FEL or ERL CW

Proton Linacs: < 10% Linear Collider: 0.01 - 1%

Beam Current, Ave. Beam Power

Storage Rings: amp, MW

Linac-Based FEL or ERL 50 μ A - 100 mA

Proton Linacs: 10 - 100 mA, 1- 10 MW

Linear Collider: few ma, 10 MW



Cavity Design Choices

- Main Choices
 - RF Frequency
 - Operating Gradient
 - Operating Temperature
 - Number of Cells
 - Cell Shapes
 - Beam Aperture
- Optimize for Capital + Operating Cost
- Best Cavity/Accelerator Performance for Least Risk
- Optimizations Involve Many Trade-offs
- Discuss parameters/dependencies
 - But not the trade-offs



Basics for Radiofrequency Cavities

 TM_{010} mode



•Add beam tube for charge to enter and exit



$$E_z = E_0 J_0 \left(\frac{2.405\rho}{R}\right) e^{-i\omega t}$$

$$H_\phi = -i \frac{E_0}{\eta} J_1 \left(\frac{2.405\rho}{R}\right) e^{-i\omega t},$$

$$\omega_{010} = \frac{2.405c}{R},$$



Phase

Electric Field Magnetic Field

Positive Surface Charge Negative Surface Charge

Surface Current





 $\pi/2$

 π

 $3\pi/2$



Medium and High Velocity Structures $\beta = v/c = 0.5 \rightarrow 1$





Basic Principle, v/c = 1



Single Cell





Multi-Cell Cavity



Squeezed Cells for v/c = 0.5



Low Velocity Structures, $\beta = v/c = 0.01 \rightarrow 0.2$





Low-Velocity Structures for Heavy lons $\beta = v/c$: 0.28 -0.62





Crab Cavities (Deflecting mode TM110)

- KEK-B
- Possibly LHC-upgrade
- Possibly Ultra-fast X-ray source



The crab crossing scheme allows a large crossing angle collision without introducing any synchrotron-betatron coupling resonances.





Figures of Merit Accelerating Voltage/Field (v = c Particles)

 For maximum acceleration need $T_{\rm cav} = \frac{d}{c} = \frac{T_{\rm rf}}{2}$

> so that the field always points in the same direction as the bunch traverses the cavity

•

$$V_{\rm c} = E_0 \left| \int_0^d e^{i\omega_0 z/c} dz \right| = dE_0 \frac{\sin\left(\frac{\omega_0 d}{2c}\right)}{\frac{\omega_0 d}{2c}} = dE_0 T.$$

Accelerating field is:





Figures of Merit for SC Cavity

- Accelerating Field and Q: E_{acc}, Q
- Stored Energy, Geometry Factor
- Peak Electric and Magnetic Field Ratios

$$-E_{pk}/E_{acc}, H_{pk}/E_{acc}$$

 Shunt Impedance, Geometric Shunt Impedance: R_a, R_a/Q

Single Cell Cavities









Figures of Merit Peak Fields

- For E_{acc} → important parameter is E_{pk}/E_{acc},
 Typically 2 2.6
- Make as small as possible, to avoid problems with field emission more later.
- Equally important is *H_{pk}/E_{acc}*, to maintain SC

- Typically 40 - 50 Oe/MV/m

- *H_{pk}/E_{acc}* can lead to premature quench problems (thermal breakdown).
- Ratios increase significantly when beam tubes are added to the cavity or when aperture is made larger.

Peak fields for low beta cavities are higher

Typical

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Epk/Eacc = 4 - 6
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Hpk/Eacc = 60 - 200 Oe/MV/m

Figures of Merit

Dissipated Power, Stored Energy, Cavity Quality (Q)

- •Surface currents ($\propto H$) result in dissipation proportional to the surface resistance (R_s) :
- •Dissipation in the cavity wall given by surface integral:

•Stored energy is: – ττ

•Define Quality (Q) as
$$Q_0 = \frac{\omega_0 U}{P_c} = 2 \pi \frac{U}{T_{rf} P_c}$$

which is $\sim 2 \pi$ number of cycles it takes to dissipate the energy stored in the cavity \rightarrow Easy way to measure Q

•
$$Qnc \approx 10^4$$
, $Qsc \approx 10^{10}$

 $\frac{dP_{\rm c}}{ds} = \frac{1}{2}R_{\rm s}|\mathbf{H}|^2$

$$P_{\rm c} = \frac{1}{2} R_{\rm s} \int_{\rm S} |\mathbf{H}|^2 \, ds$$

$$\longrightarrow U = \frac{1}{2}\mu_0 \int_{\mathcal{V}} |\mathbf{H}|^2 \, dv$$

Since the time averaged energy in the electric field equals that in netic field, the total energy in the cavity is given by

$$U = \frac{1}{2}\mu_0 \int_{\mathcal{V}} |\mathbf{H}|^2 \, dv = \frac{1}{2}\epsilon_0 \int_{\mathcal{V}} |\mathbf{E}|^2 \, dv,$$

where the integral is taken over the volume of the cavity.

the dissipated power
$$P_{\rm c} = \frac{1}{2} R_{\rm s} \int_{\rm S} |{\bf H}|^2 \, ds,$$

where the integration is taken over the interior cavity surface.

$$Q_{0} = \frac{\omega_{0}U}{P_{c}}, \qquad \qquad Q_{0} = \frac{\omega_{0}\mu_{0}\int_{V}|\mathbf{H}|^{2} dv}{R_{s}\int_{S}|\mathbf{H}|^{2} ds}$$

The Q_0 is frequently written as

$$Q_0 = \frac{G}{R_{\rm s}},$$

where

$$G = \frac{\omega_0 \mu_0 \int_{\mathbf{V}} |\mathbf{H}|^2 \, dv}{\int_{\mathbf{S}} |\mathbf{H}|^2 \, ds}$$

For the pill-box TM_{010} mode we find

1

,

$$U = E_0^2 \pi d\epsilon_0 \int_0^R \rho J_1^2 \left(\frac{2.405\rho}{R}\right) d\rho$$
$$P_c = \frac{R_s E_0^2}{\eta^2} \left\{ 2\pi \int_0^R \rho J_1^2 \left(\frac{2.405\rho}{R}\right) d\rho + \pi R dJ_1^2 (2.405) \right\}$$

$$\int \rho J_{\nu}^2(\alpha \rho) \, d\rho = \frac{\rho^2}{2} \left[J_{\nu}^2(\alpha \rho) - J_{\nu-1}(\alpha \rho) J_{\nu+1}(\alpha \rho) \right]$$

$$U = \frac{\pi\epsilon_0 E_0^2}{2} J_1^2 (2.405) dR^2$$

$$P_c = \frac{\pi R_s E_0^2}{\eta^2} J_1^2 (2.405) R(R+d)$$

$$G = \frac{\omega_0 \mu_0 dR^2}{2(R^2 + Rd)} = \eta \frac{2.405d}{2(R+d)} = \frac{453 \frac{d}{R}}{1 + \frac{d}{R}} \Omega.$$

G is indeed independent of the cavity's size.

$$G = 257 \ \Omega. \qquad \qquad \frac{d}{R} = \frac{\pi}{2.405}$$

If
$$R_{\rm s} = 20 \ {\rm n}\Omega$$
 $Q_0 = \frac{G}{R_{\rm s}} = 1.3 \times 10^{10}$.

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A typical length of d = 10 cm requires a cavity radius R of 7.65 cm or, equivalently, a resonant frequency of 1.5 GHz. For operation at $V_c = 1$ MV the following results are found to apply:

$$E_{\text{acc}} = \frac{V_{\text{c}}}{d} = 10 \text{ MV/m}$$

$$E_{\text{pk}} = E_0 = \frac{\pi}{2} E_{\text{acc}} = 15.7 \text{ MV/m}$$

$$H_{\text{pk}} = 30.5 \frac{\text{Oe}}{\text{MV/m}} E_{\text{acc}} = 305 \text{ Oe}$$

$$U = E_0^2 \frac{\pi \epsilon_0}{2} J_1^2 (2.405) dR^2 = 0.54 \text{ J}$$

$$P_{\text{c}} = \frac{\omega U}{Q_0} = 0.4 \text{ W}.$$

$$\frac{E_{\rm pk}}{E_{\rm acc}} = \frac{\pi}{2} = 1.6$$
$$\frac{H_{\rm pk}}{E_{\rm acc}} = 2430 \frac{\rm A/m}{\rm MV/m}$$

adamsee

Figures of Merit Shunt Impedance (R_a)

• Shunt impedance (R_a) determines how much acceleration one gets for a given dissipation (analogous to Ohm's Law)

$$R_{\rm a} = \frac{V_{\rm c}^2}{P_{\rm c}}$$

 \rightarrow To maximize acceleration, must maximize shunt impedance.

Another important figure of merit is

$$\frac{R_{\rm a}}{Q_0} = \frac{V_{\rm c}^2}{\omega_0 U},$$

•Ra/Q only depends on the cavity geometry → Cavity design impacts mode excitation

Evaluation - Analytic Expressions

1.5 GHz pillbox cavity, R = 7.7 cm, d = 10 cm

$$\frac{R_{\rm a}}{Q_0} = \frac{V_{\rm c}^2}{\omega_0 U},$$

$$\frac{R_{\rm a}}{Q_0} = 150 \ \Omega \ \frac{d}{R} = 196 \ \Omega$$

For Cu: $R_s = 10 \text{ mohm} \rightarrow Q = 25,700, R_a = 5 \text{ Mohm}$ For Nb: $R_s = 10 \text{ nohm} \rightarrow Q = 25,700,000,000, R_a = 5 \text{ Tohm!}$

Real Cavities Codes

- Adding beam tubes reduces R_a/Q by about x2 => for Cu cavities use a small beam hole.
- Peak fields also increase.
 - Can be a problem for high gradient cavities
- Analytic calculations are no longer possible, especially if cavity shape is changed to optimize peak fields.
- \rightarrow Use numerical codes.
- E.g., MAFIA, MicrowaveStudio, SuperLans, CLANS, Omega3P....

0.11 V/pc

89 Ω/cell

Quantity	Cornell SC 500 MHz	Pillbox
G	$270 ext{ ohm} \Omega$	257Ω
$R_{ m a}/Q_0$	88 ohm/cell	$196 \ \Omega/\mathrm{cell}$
$E_{\rm pk}/E_{\rm acc}$	2.5	1.6
$H_{\rm pk}/E_{\rm acc}$	52 Oe/MV/m	$30.5 ~\mathrm{Oe}/(\mathrm{MV/m})$

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0.11 V/pc

Copper Cavity Example **CW** and Low Gradient

$$Rs = \sqrt{(\pi f \,\mu_0 \,\rho)}$$

f = RF frequency $\rho = DC$ resistivity $\mu_0 = permeability of free space$

 $\rightarrow P_{diss} = 250 \text{ kW}$

- Example: Assume we make this cavity out of copper
- Want to operate CW at 500 MHz and
- 1 MV (3 MV/m) R/Q = 89 Ohm

89 Ω/cell R83 R20 240 • $R_{\rm s} = 6$ mohm mm $\rightarrow Q = 45,000$ (b) Superconducting B-Factory Cell Shape $\rightarrow R_a = 4$ Mohm

This would result in a overheating of copper cell. Water-cooled copper cavities at this frequency can dissipate about 40 kW.

(CW) copper cavity design is primarily driven by the requirement that losses must be kept small.

Minimizing Losses

Optimizing CW Copper Cavities High Current Application

- Use small beam tubes
- Use reentrant design to reduce surface magnetic currents.
- $\rightarrow R_a/Q = 265 \text{ Ohm}$

PEP-II: 476 MHz

- $\rightarrow P_{diss} = 80 \text{ kW} @ 3 \text{ MV/m}$
- Still have to reduce voltage to 0.7 MV.

R/Q (fundamental) = 265 Ω/cell

Superconductivity

0,15 2 0,125 0,10 0,075 0,05 0,025 6-5 R 0,00 4'10 120 924'30 4 '40 4'00 surement of superconductivity by Ka

The Convergence of Classical Concepts circa 1900

Figure 1-2. Heike Kamerlingh Onnes. Coursesy AIP See . E. hr Library and

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Elementary Solid State : Electrons in Solids

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Electron Energy Levels

Normal conductor

Electron-Phonon Interaction

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Superconductivity

For T > 0K, have some excitation of "normal" electrons

$$n_{\rm normal} \propto \exp\left(-\frac{\Delta}{k_{\rm B}T}\right)$$

→ Two Fluid Model

Normal conductor Superconductor (electrons form Cooper pairs) T = 0 K

Simplified Explanation for Zero Resistance

- NC
 - Resistance to flow of electric current
 - Free electrons scatter off impurities, lattice vibrations (phonons)
- SC
 - Cooper pairs carry all the current
 - Cooper pairs do not scatter off impurities due to their coherent state
 - Some pairs are broken at T>0K due to phonon interaction
- But supercurrent component has zero resistance

Superconductors: RF Resistance

- DC resistance is zero because NC electrons are shorted out by SC ones.
- RF resistance small but finite because Cooper pairs have inertia → nc

 $R_{\rm s} = A_{\rm s} \omega^2 \exp\left(-\frac{\Delta(0)}{k_{\rm B}T}\right)$

More resistance the more the sc pairs are jiggled around are excited


Low Field Frequency and Temperature Dependence of Rs

$$R_{s} = A(\lambda_{L}, \xi_{0}, l) f^{2} e^{(-\Delta_{0}/kT)} \text{ for } T < 0.5$$

Tc

 λ_L London penetration depth

 ξ_0 Coherence length of Cooper pairs

v_F Fermi velocity

 Δ_0 Energy gap

1 electron mean free path

Tc = SC transition temperature

$$R_{bcs} = 3x \quad 10^{-4} \left[\frac{f(GHz)}{1.5}\right]^{2} \left(\frac{1}{T}\right) e^{-(17.67/T)}$$

Good fitting function



Cavity Q₀

- 120 C bake
- Lowers electron mean free path and increases BCS Q





Superconducting Cavity

 Recalculate P_{diss} with SC Nb at 4.2 K, 1 MV, and 500 MHz.

$$Q = 2 \times 10^9 (R_s \approx 15 \text{ n}\Omega)$$

- → $R_{\rm a}$ = 5.3 x 10¹¹
- $\rightarrow P_{diss} = 1.9 \text{ W!}$
- → P_{ac} = 660 W = AC power (Frig. efficiency = 1/350)
- → Include cryostat losses, transfer lines, etc.
- → P_{ac} increases, but is still 10-100 times less than that of Cu cavities.

0.11 V/pc



Superconducting B-Factory Cell Shape



A challenge of the SC option is cryogenics

Refrigerator efficiencies are low

And one has to add other heat contributions from conduction, radiation, helium distribution.

Carnot efficiency of frig and technical efficiency of frig machinery

$$\eta_{\text{Carnot}} = \frac{4.5}{300 - 4.5} = 0.015$$

$$\eta_{technical} = 0.20$$

$$\eta_{total} = 0.003 = 1/333$$



SRF Requirements & Limitations

• Cryogenic system.

Real Estate Gradient lower than active gradient

(0.5 -> 0.7) Eactive copper cavities 0.8 Eactive



Hi Tech: Ultra-clean preparation and assembly required

Max Eacc = 50 MV/m More Later





SC Advantages

- Power consumption is much less → operating cost savings, better conversion of ac power to beam power.
- CW operation at higher gradient possible → Less klystron power required → capital cost saving
- Need fewer cavities for CW operation → Less beam disruption



Design Comparison



273 mm



CW RF Cavities for Storage Rings



Superconducting Cavity: CESR-III

Copper Cavity: PEP-II



Fundamental differences due to difference in wall losses



(Some) Further SC Advantages

- Freedom to adapt design better to the accelerator requirements allows, <u>for example</u>, the beamtube size to be increased:
 - Reduces the <u>interaction</u> of the beam with the cavity (scales as size³) →
 The beam quality is better preserved (important for, e.g., FELs).
 - HOMs are removed more easily → better beam stability → more current accelerated (important for, e.g., Bfactories)
 - Reduce the amount of beam scraping
 → less activation in, e.g., proton machines (important for, e.g., SNS, Neutrino factory)





Additional Design Aspects for Multi-cell Cavities



(a)



Standing Wave Mode









Dispersion Relation







Circuit Model of MultiCells



: Sketch of the electric field lines of the $\pi\text{-mode}$ of a 5-cell :



Equivalent circuit for a 4-cell cavity with beam tubes.





define
$$\omega_0^2 = 1/LC$$
, $k = C/C_k$, $\gamma = C/C_b$,

Solve the circuit equations for mode frequencies Dispersion Relation

$$\left(\frac{f_m}{f_0}\right)^2 = 1 + 2k \left[1 - \cos\left(\frac{m\pi}{N}\right)\right]$$

If we measure $f^{(N)}$ and $f^{(1)}$, this becomes

$$k = \frac{\frac{1}{2} \left[\left(f^{(N)} \right)^2 - \left(f^{(1)} \right)^2 \right]}{2 \left(f^{(1)} \right)^2 - \left(f^{(N)} \right)^2 \left[1 - \cos \left(\pi/N \right) \right]}$$

Mode spacing increases with stronger cell to cell coupling k Mode spacing decreases with increasing number of cells N



Field Flatness

- Stronger cell-to-cell coupling (k) and smaller number of cells N means
 - Field flatness is less sensitive to mechanical differences between cells





Tuning for Right Frequency and Field Profile



In Addition to EM Properties Mechanical Properties Are Also Important to Cavity Design

- Cavity should not collapse or deform too much under atmospheric load
- Shape
 - avoid flat regions-
 - Elliptical profile is stronger
- Choose sufficient wall thickness
- Use tuner to bring to right frequer



LORENTZ FORCE DETUNING .

The rf magnetic field in a cavity interacts with the rf wall current resulting in a Lorentz force which can become important at high accelerating fields The radiation pressure,

$$P_{\rm L} \propto \mu_0 H^2 - \epsilon_0 E^2,$$

causes a small deformation of the cavity shape resulting in a shift of the cavity resonant frequency:

$$\Delta f \propto (\epsilon_0 E^2 - \mu_0 H^2) \Delta V.$$

Here ΔV is the change in the volume of the cavity region that is undergoing deformation. The typical coefficient is a few $Hz/(MV/m)^2$.



Cavity Performance Characterization

Most Important : Q vs E curve





Critical Fields

- Superconductors only remain in the superconducting state if the applied field is less than the critical magnetic field H_c (2000 Oe for Nb for DC)
- But! Phase transition requires some time (1 μ s?) to nucleate sc-nc transition.
- \rightarrow For RF can exceed H_c up to the superheating field.

For typical v = c cavities this is achieved at an accelerating field of $E_{\rm acc} \approx 50$ MV/m.



DC Critical Magnetic fields







Meissner Effect

- Magnetic fields are screened by surface currents in the SC → perfect diamagnetism
- SC goes normal conducting when the energy needed for shielding exceeds that gained by being superconducting.





Levitation by Meissner Effect



Critical RF Magnetic Field

- What is the relationship between the RF critical magnetic field and the familiar DC critical magnetic fields?
- Is Hrf
 - $\ H_{c1}, H_{c}, H_{sh}?$
 - How does it depend on temperature?
 - How does it depend on
 - Ginzburg-Landau parameter $\kappa = \lambda/\xi$?
 - Nb: $\kappa \sim 1$, Nb3Sn: $\kappa \sim 20$..





Cornell Experimental Status (1996) Measured RF Critical Field for : Nb₃Sn Using High Pulse Power (Calibrated results with Nb)



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Theoretical RF Electric Field

- No known theoretical limit
- In SC test cavities, SC survives up to

 Epk = Pulsed 220 MV/m
 145 MV/m CW over cm² area
- Single cell 1300 MHz accelerator cavity to Epk = 120 MV/m, CW (55 x 2.2)



Evolution of Cavity Gradients (1970 – 2009)

And SRF Technology Over 4 Decades

Steady progress in Gradients due to basic understanding of limiting phenomena and invention of effective cures



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Thermometry Has Been the Key







Cavity Performance Characterization

Most Important : Q vs E curve









Solution to Multipacting



Electrons drift to equator Electric field at equator is ≈ 0 →MP electrons don't gain energy →MP stops



Heating at sub-mm size defects leads to quench of superconductivity





Museum of Defects Causing Quench





0.2 mm Ta defect, 15 MV/m

50 $\mu m,$ with S, Ca, Cl, and K, 11 MV/m



A chemical stain 440 μ m in diameter. K, Cl, and P, 3. 4 MV/m







50 micron Cu particle fell into cavity

500 x 200 microns pit

Sub-mm Nb welding ball, 72 avoidable

Improve Bulk Thermal Conductivity (and RRR) by raising purity to avoid Ouench



 κ_T scales \approx linearly with RRR.


Niobium Purification





Interstitial O, N and C are the major impurities limiting Nb RRR



Field Emission







Museum of Known Field Emitters 0.5 to 10 microns Note the sharp features on the Particles.



(a) Sub-micron field emitting particles found on sample prepared with 9-cell cavity

(b) Al particle found at a field emission site in the dc field emission scanning apparatus and subsequently analyzed with the SEM

(c) Field emitting particle found with thermometry followed by dissection of a 1.5 GHz cavity. Carbon, oxygen, iron, chromium, and nickel were among the foreign elements detected



Vertical Tests Eacc (MV/m)





100 atm jet water rinsing







HPR and Assembly at CornellH. Padamsin Class 100 Clean Room< 100 particles/cu.ft</td>> 1 μ m







<u>All</u> RF Processing of Field Emission Means to Burn off Remaining Electron Emitters by Sparking RF Processing Can be Enhanced With High Power RF

1 MW, 200 µsec pulses





P10



CW Low Power RF Processing of Carbon Emitter Planted in 6 GHz Cavity





Push for High Gradients : Cornell, FNAL, DESY Collaboration Gradients > 25 MV/m in Three 5-cell 1300 MHz Cavities











Electropolishing Setup at DESY



Lutz Lilje DESY -MPY-



15.07.2006

see



Best Performance Results





Outstanding Issues for Highest Gradient Applications: e.g. ILC

- Yield at 35 MV/m is low
- Spread is high:
 - Quench
 - Field emission
- Best 9-cell Cavities About one dozen





Vertical Tests Eacc (MV/m)





9-cell DESY Cavities Prepared by EP and Baking





Impact of SRF on Accelerators for Science Existing and Future Applications

- Low energy nuclear physics, for nuclear shape, spin, vibration...
 - Heavy ion linacs
- Medium energy nuclear physics, structure of nucleus, quark-gluon physics
 - Recirculating linac
- Nuclear astrophysics, for understanding the creation of elements
 - Facility for rare isotope beams (FRIB)
- X-Ray Light Sources for life science, materials science & engineering
 - Storage rings, free electron lasers, energy recovery linacs
- Spallation neutron source for materials science and engineering, life science, biotechnology, condensed matter physics, chemistry
 - High intensity proton linac
- Future High Intensity Proton Sources for
 - Nuclear waste transmutation, energy amplifier, power generation from Thorium
- High energy physics for fundamental nature of matter, space-time
 - Electron-positron storage ring colliders, linear collider, proton linacs for neutrinos



SRF Has Become a Core Technology Worldwide for a Variety of Accelerators Total > 7 GV installed (>3 GV still in operation: CEBAF, SNS, FLASH) LEP-II was 3.5 GV, later de-commissioned for LHC

- HEP
 - Now: LHC, CESR-TA, KEK-B, Beijing Tau-charm Factory
 - Future: LHC-crab-crossing, ILC, Project X, CERN-SPL, Neutrino Factory, JPARC-Upgrade (neutrino beam line) Muon Collider
- NP
 - Low Energy
 - Now: ATLAS (Argonne), ALPI (INFN Legnaro Italy), ISAC-II (TRIUMF), IUAC (Delhi)
 - Medium Energy Nuclear-Astrophysics
 - Now: CEBAF, 12GeV Upgrade,
 - Nuclear Astrophysics
 - Future: FRIB (MSU), ISAC-II (TRIUMF), Spiral-2, CERN ISOLDE Upgrade, Eurisol, RHIC-II, eRHIC, ELIC
- BES X-rays
 - Now: FLASH, X-FEL, CHESS, Canadian Light Source, DIAMOND, SOLEIL, Taiwan Light Source, Beijing Light Source (Tau-charm Factory), Shangai Light Source, Jlab-FEL/ERL, Rossendorf-FEL
 - Future: NSLS-II, Cornell-ERL, KEK-ERL, BESSY-ERL, WIFEL (Wisconsin), ARC-EN-CIEL, Pohang Light Source, Peking University,...
- BES: Neutron Sources
 - SNS, SNS upgrade,
 - Future: ESS (Sweden)
- Other High Intensity Proton Sources for
 - INFN, KAERI, Indian Laboratories at Indore, Mumbai and Kolkata