



Modelling, experimentation and scaling of solar hydrogen generation devices

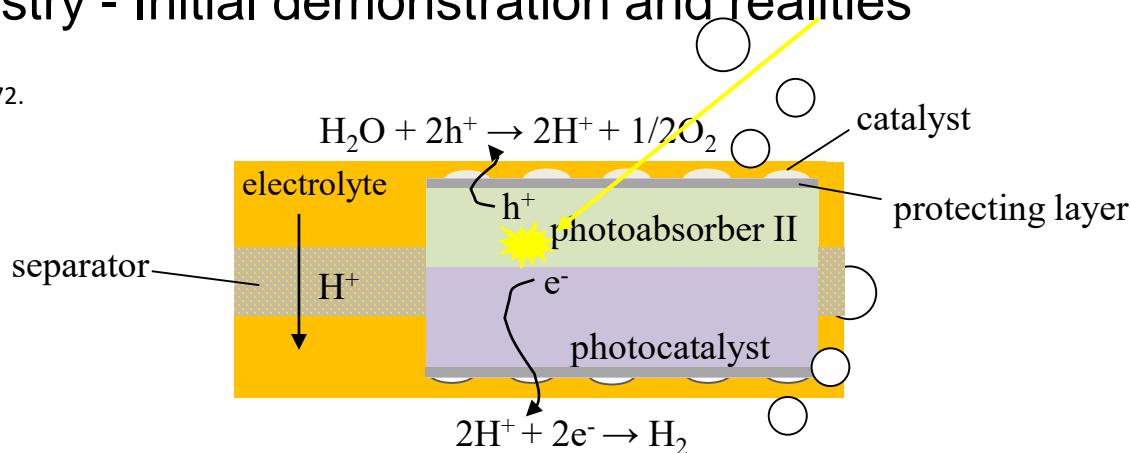
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Photo-Electrochemical Approach

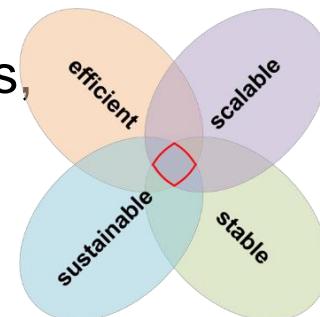
- Photoelectrochemistry - Initial demonstration and realities

Fujishima et al., *Nature*, 238, 1972.

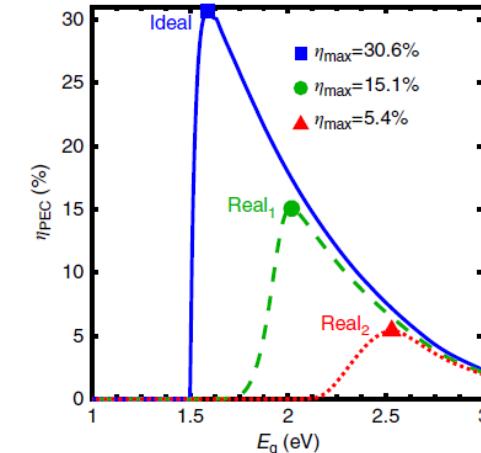


- Stringent material requirements hinder implementation
→ Functional decoupling into multiple materials

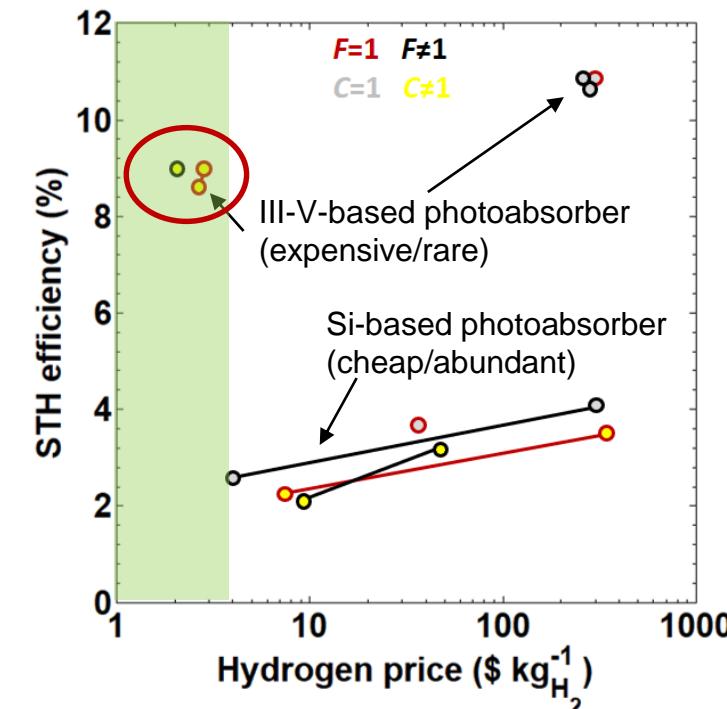
- **Challenges:** Component integration for practical devices,
few successful implementations



- **Economic driver:** Requires **high power density**
→ Achieved through irradiation concentration
→ Thermal management critical



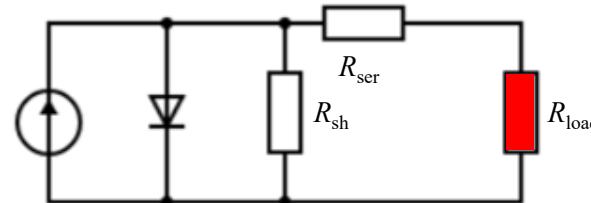
Fountaine et al., *Nature Com.*, 7, 2016



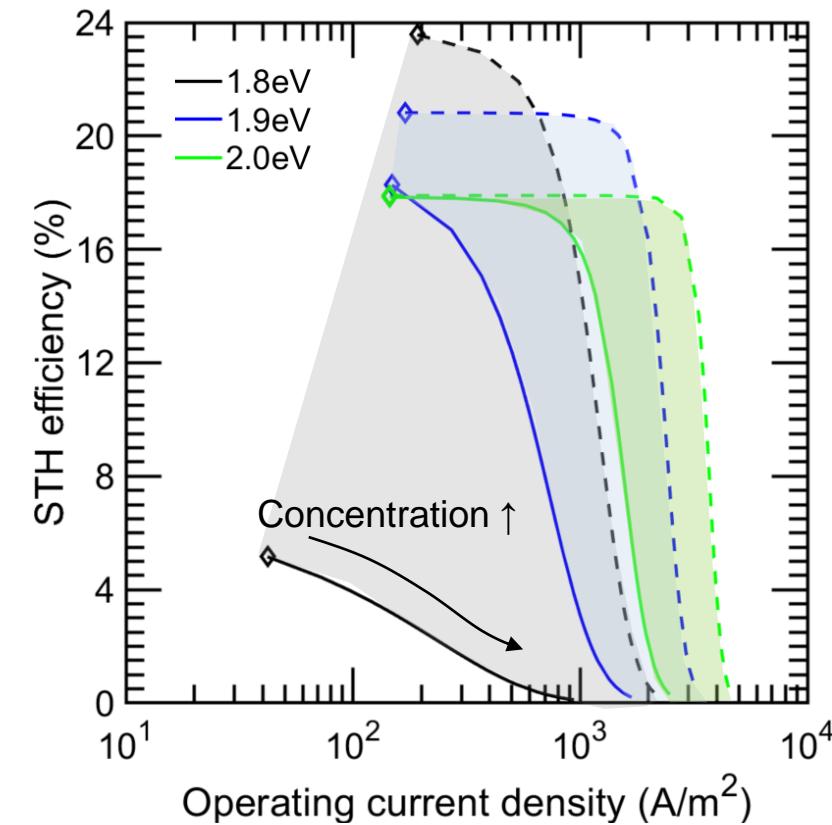
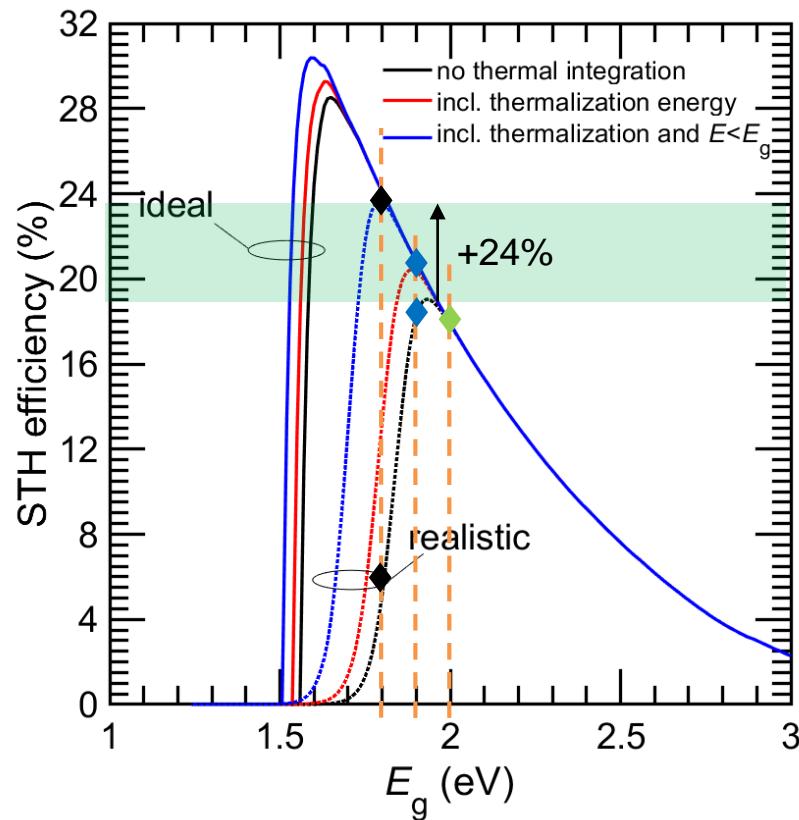
Thermal Integration

- Engineering to go beyond the perceived limits:

Tembhurne, Nandjou, Haussener, *Nature Energy*, doi: 10.1038/s41560-019-0373-7, 2019



Solid lines: no thermal integration
Dashed lines: with thermal integration



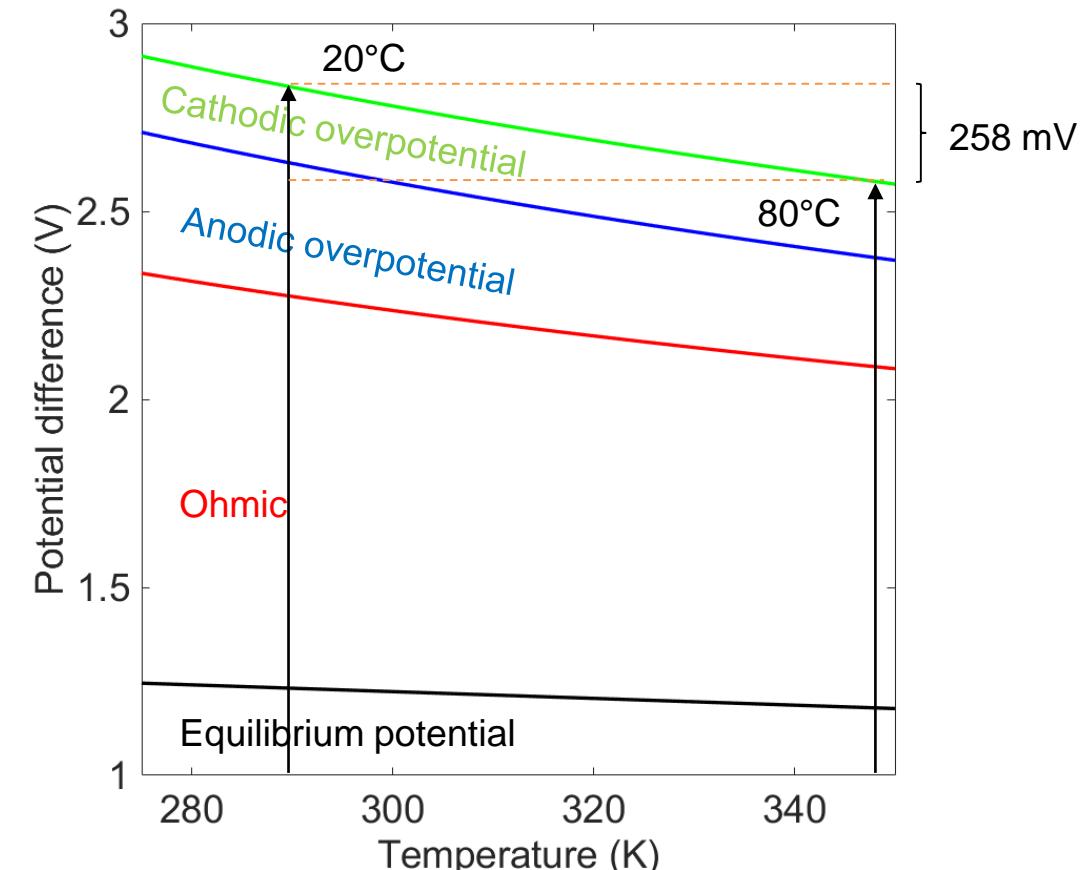
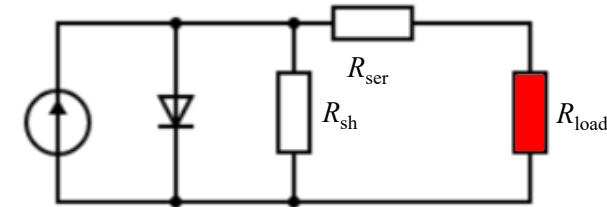
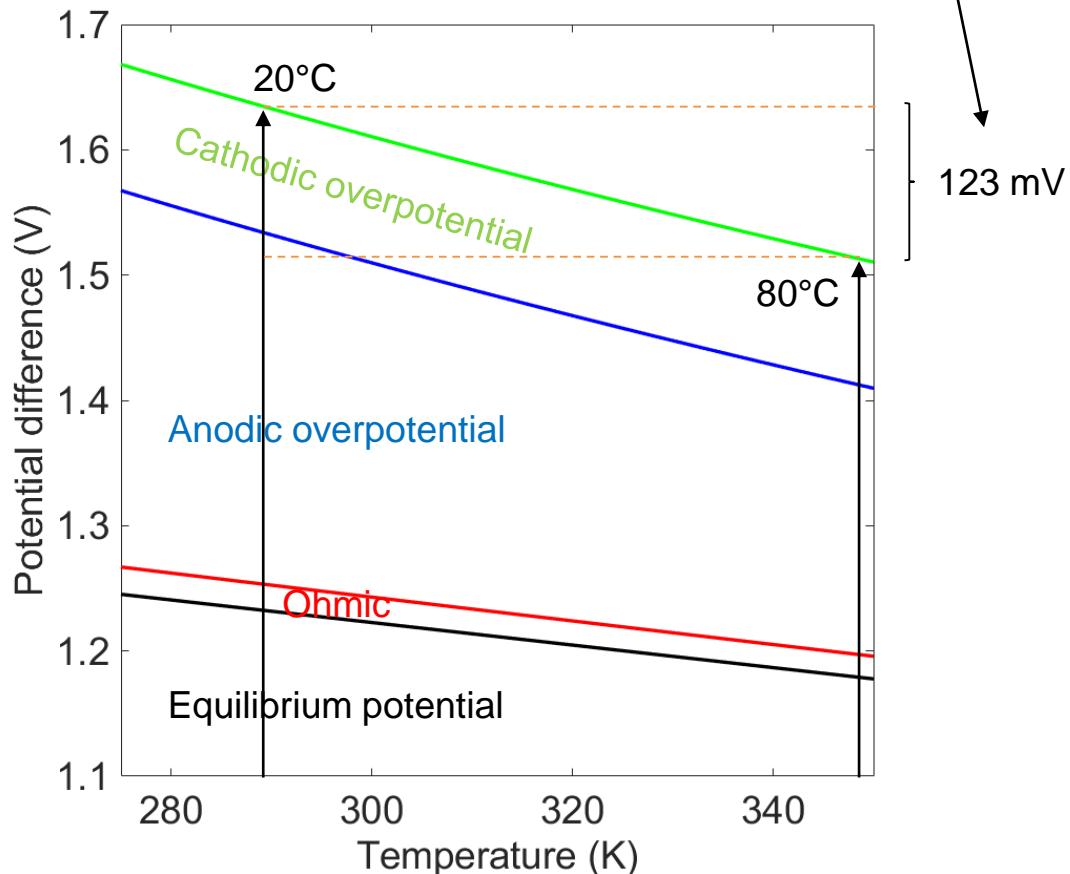
High electrochemical and power densities enabled by thermal integration

Thermal Integration

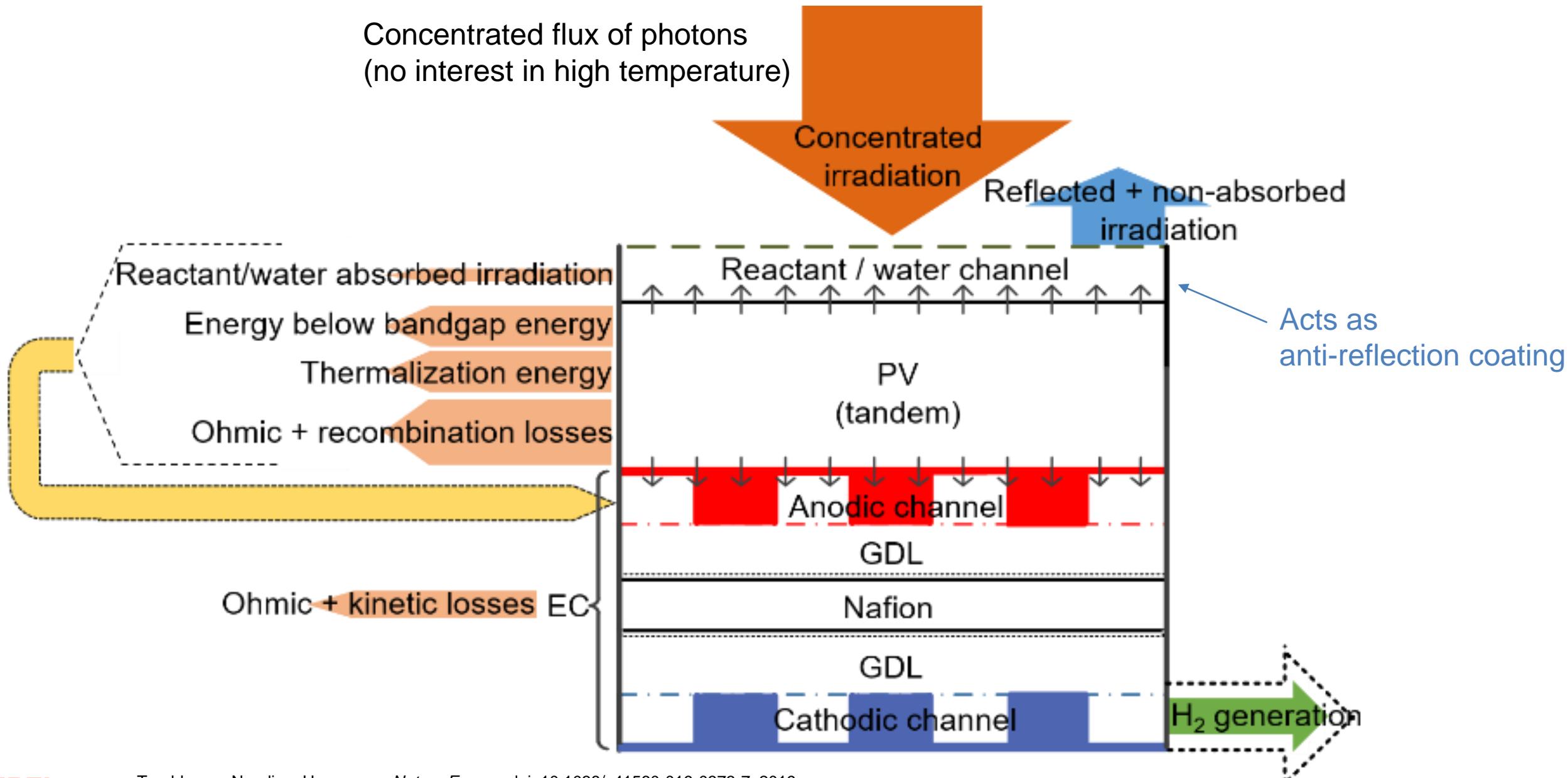
- Thermal benefit

@ 20 mA/cm²

A decade of catalysis research



Conceptual Device Design



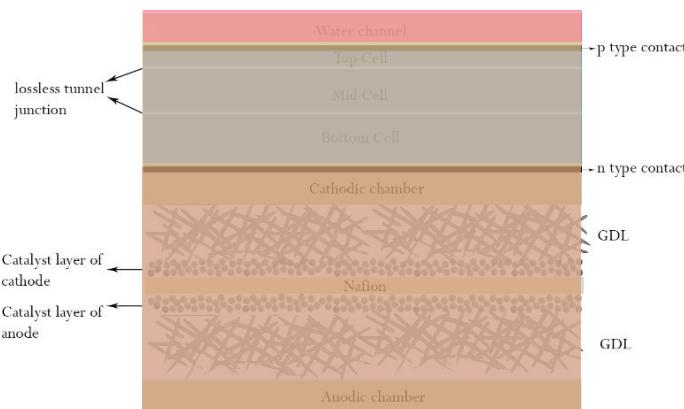
2D Modeling

- How to design a device that has never been considered before?
→ Coupled multi-physics simulations

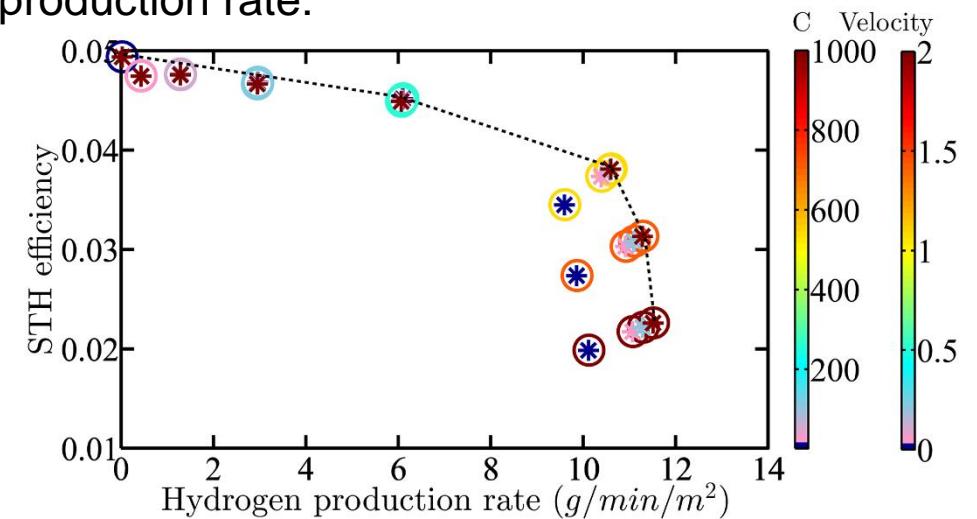
Electromagnetic wave propagation
Semiconductor charge conservation / transfer
Electrodes/electrolyte charge conservation / transfer
(Reactive) fluid flow
Energy conservation / heat transfer

$$\rho C_p \mathbf{u} \cdot \nabla T = \nabla \cdot (k_{\text{th}} \nabla T) + Q$$

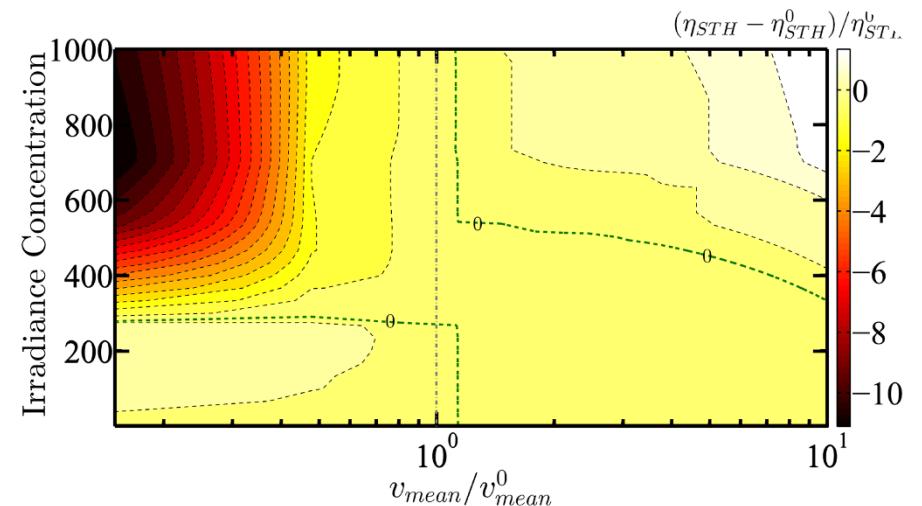
$$Q = Q_W + Q_{\text{TH}} + Q_R + Q_M + Q_{\text{PV}} + Q_{\text{EC}}$$



Efficiency vs. production rate:

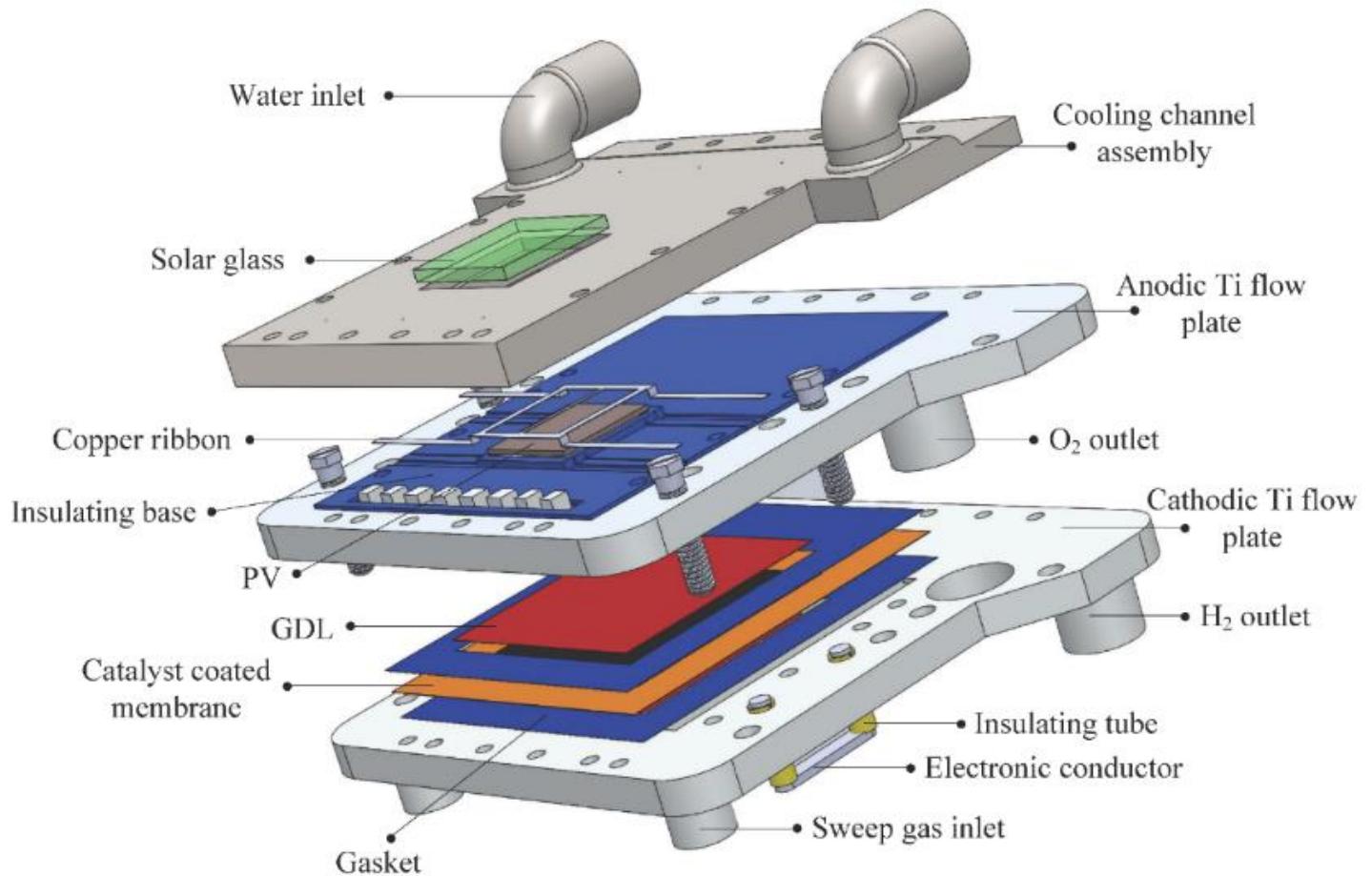


Efficiency improvement for varying operating conditions:

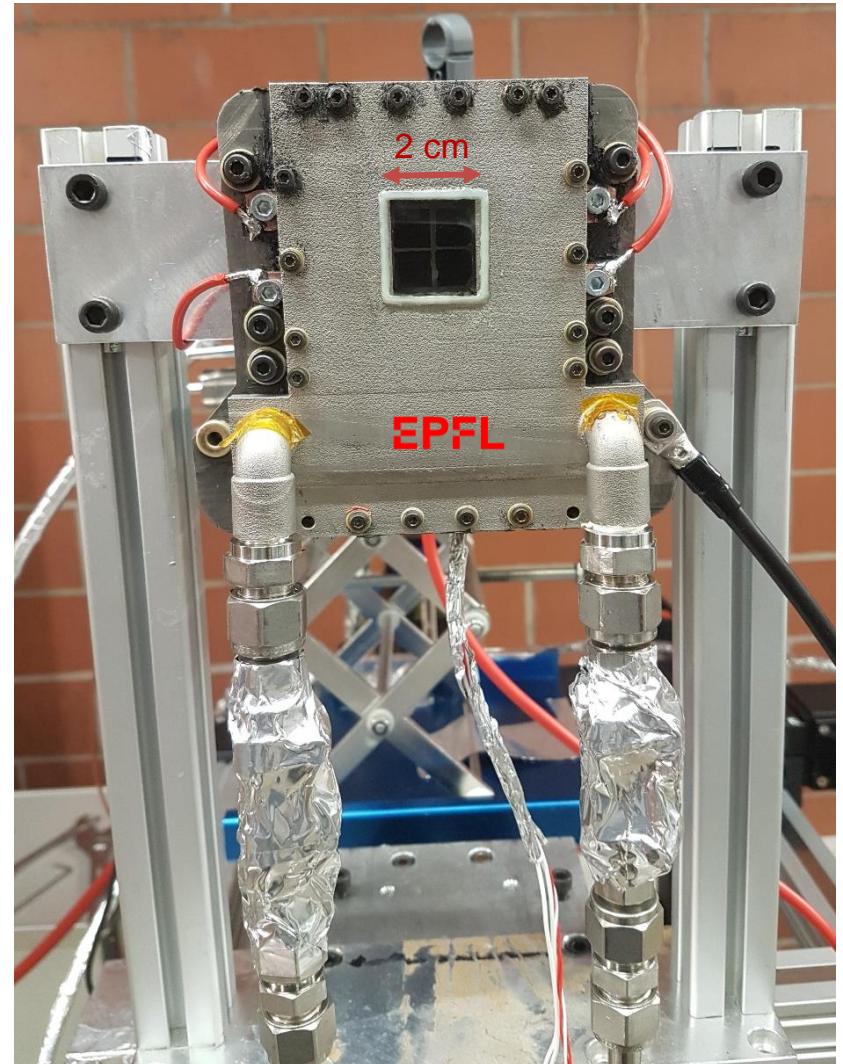


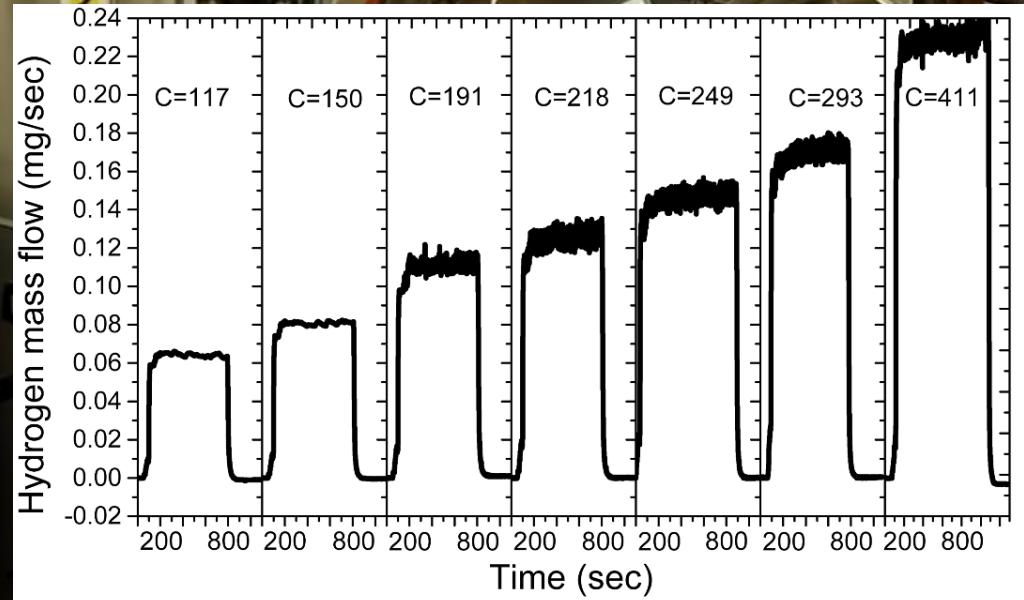
CPEC Design

- Implementation:



US Patent 62/376923
EP Patent 16020308.9





Output power of PEC at 474 kW/m^2 : 27 W

Current density in electrolyzer component: 0.88 A/cm^2

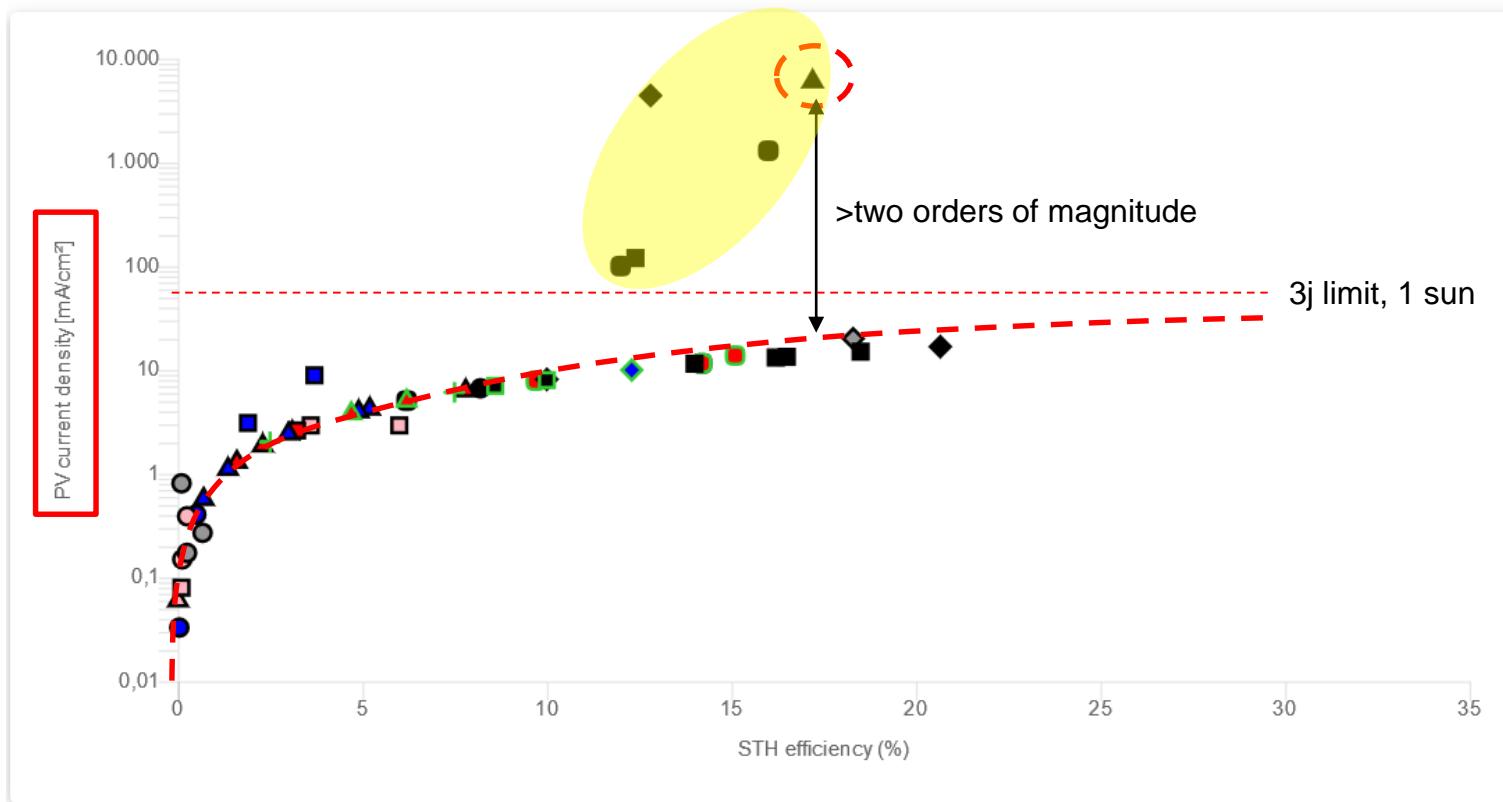
Current density in photoabsorber component: 6.04 A/cm^2

Efficiency: 17.1% solar-to-fuel

Tembhurni, Nandjou, Haussener, *Nature Energy*, doi: 10.1038/s41560-019-0373-7, 2019

Comparison

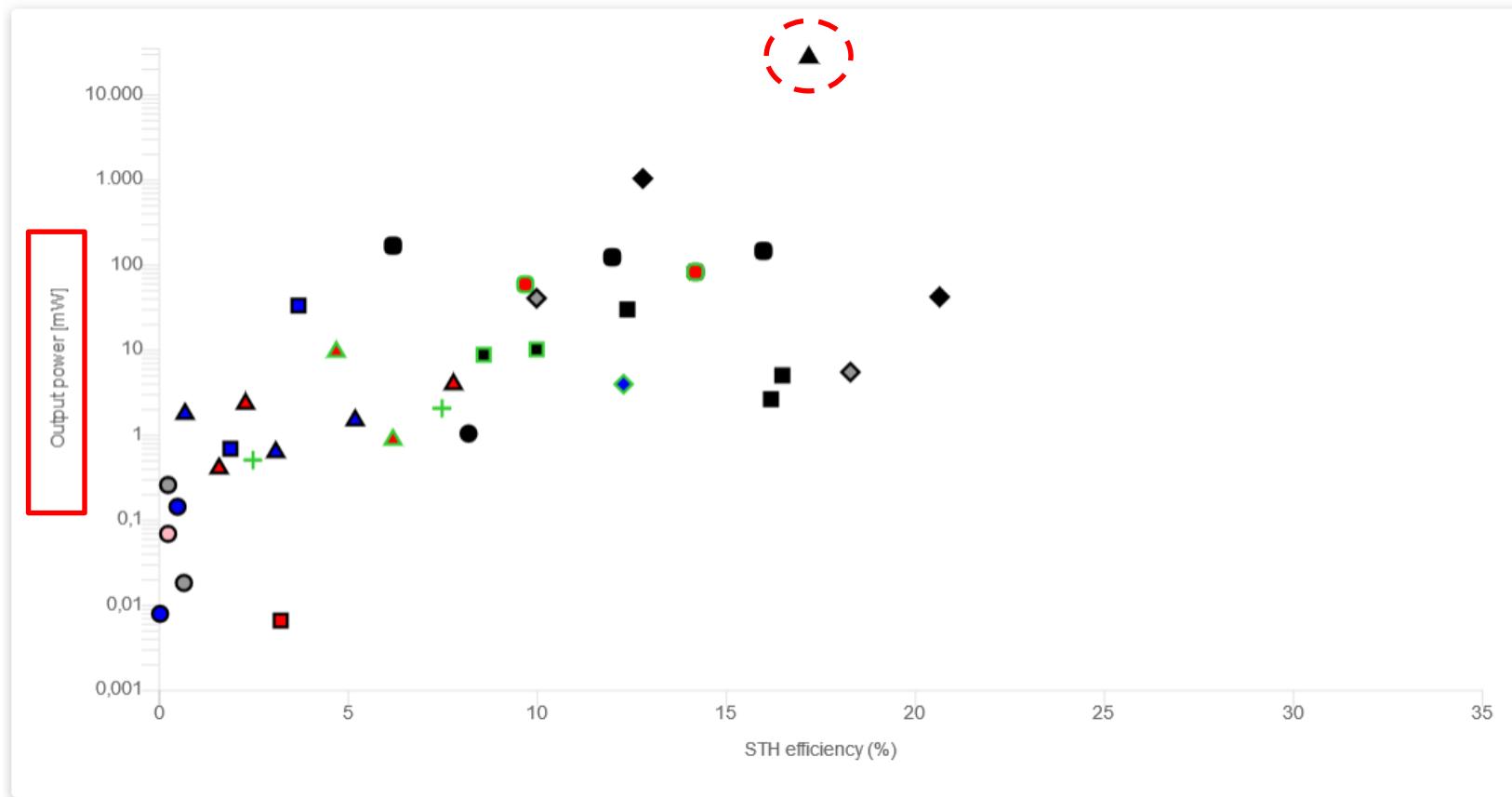
- Dynamic and online tool: – <http://specdc.epfl.ch/>



LEGEND			
Fill color - PV / photoabsorber material	Boundary color - EC material	Symbol shape - PV / photoabsorber and EC configuration	
All III-V	Rare metal-based (expensive)	○	2J, integrated PVs and catalyst
Partial III-V	Abundant (cheap)	□	2J, integrated PVs, wired catalyst
All Si		◊	2J, non-integrated PVs or catalyst
Partial Si		+	3J, integrated PVs and catalyst
Oxides and others		△	3J, integrated PVs, wired catalyst
		○	3J, non-integrated PVs or catalyst

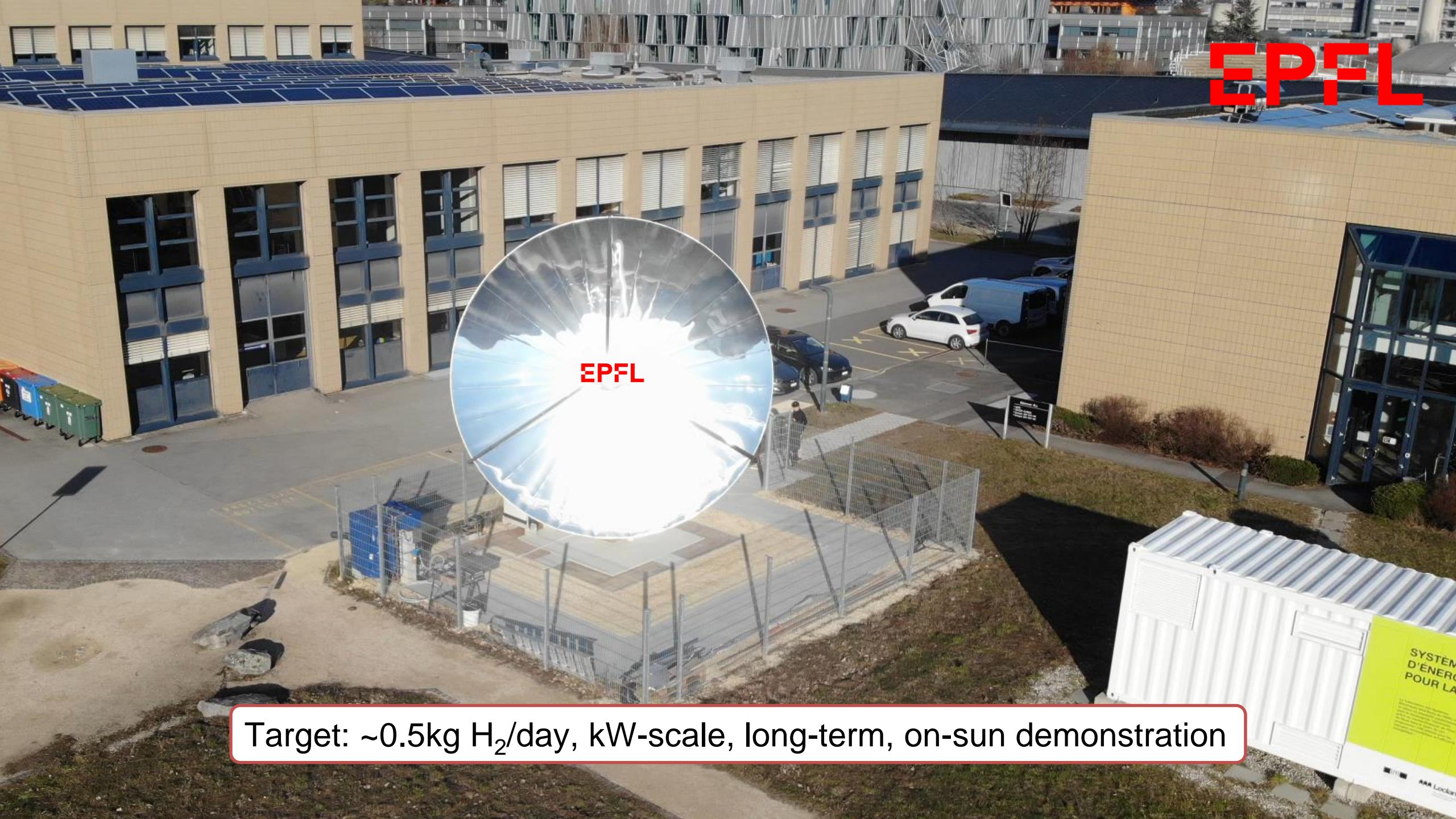
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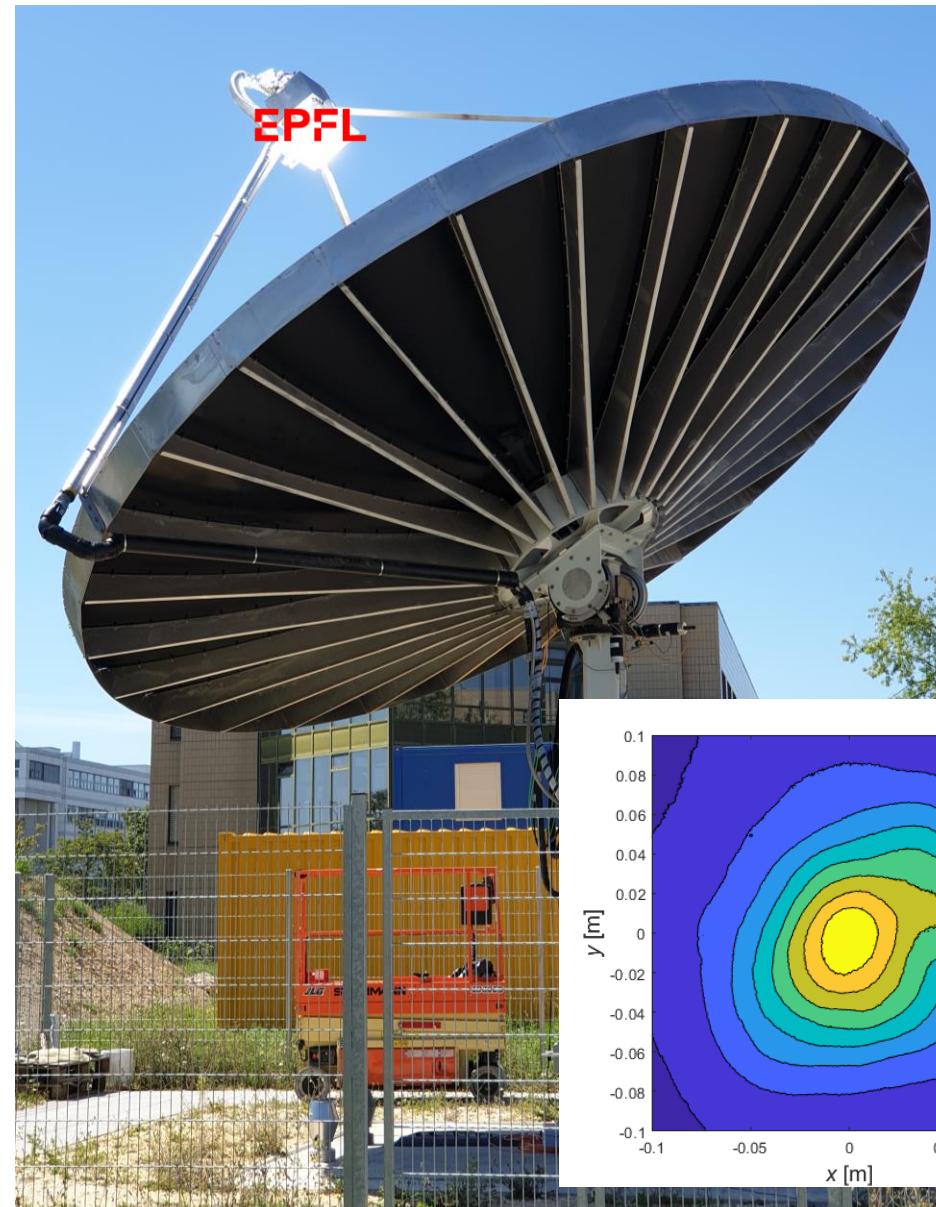
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EPFL



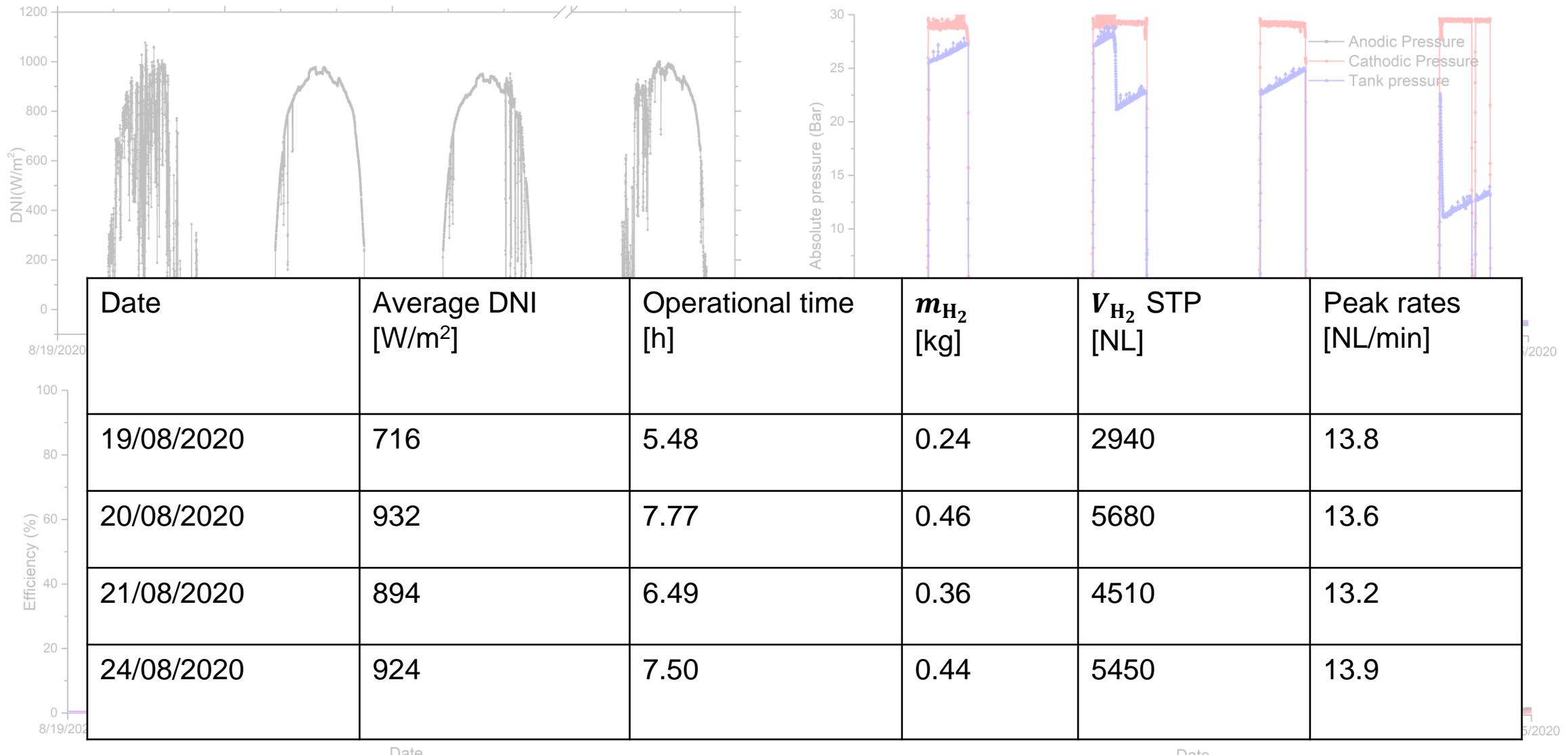
Target: ~0.5kg H₂/day, kW-scale, long-term, on-sun demonstration

Reactor and System in Operation



Integrated System Test

- Full operation over multiple days in varying meteorological conditions



Dynamic Process Model

- Generic system model developed in gPROMS ModelBuilder, parameters inspired by our installation

Electrolyser stack

$$\eta_{\text{kinetic}} = \frac{RT_{\text{EC}}}{\alpha_{\text{ano}} n_e F} \ln\left(\frac{i_{\text{cell}}}{i_{\text{o,ano}}}\right) + \frac{RT_{\text{EC}}}{\alpha_{\text{cat}} n_e F} \ln\left(\frac{i_{\text{cell}}}{i_{\text{o,cat}}}\right)$$

$$\sigma_m = (0.00514 \lambda_m - 0.00326) \exp\left(1268\left(\frac{1}{303} - \frac{1}{T_{\text{EC}}}\right)\right)$$

$$C_{\text{EC}} \frac{dT_{\text{EC}}}{dt} = Q_{\text{gen}} - Q_{\text{loss}} - Q_{\text{fluid,a}} - Q_{\text{fluid,c}}$$

$$\frac{dM_i}{dt} = x_{\text{inlet},i} \dot{m}_{\text{inlet}} - x_{\text{outlet},i} \dot{m}_{\text{outlet}} + M_{w,i} v_i R_{\text{rxn}}$$

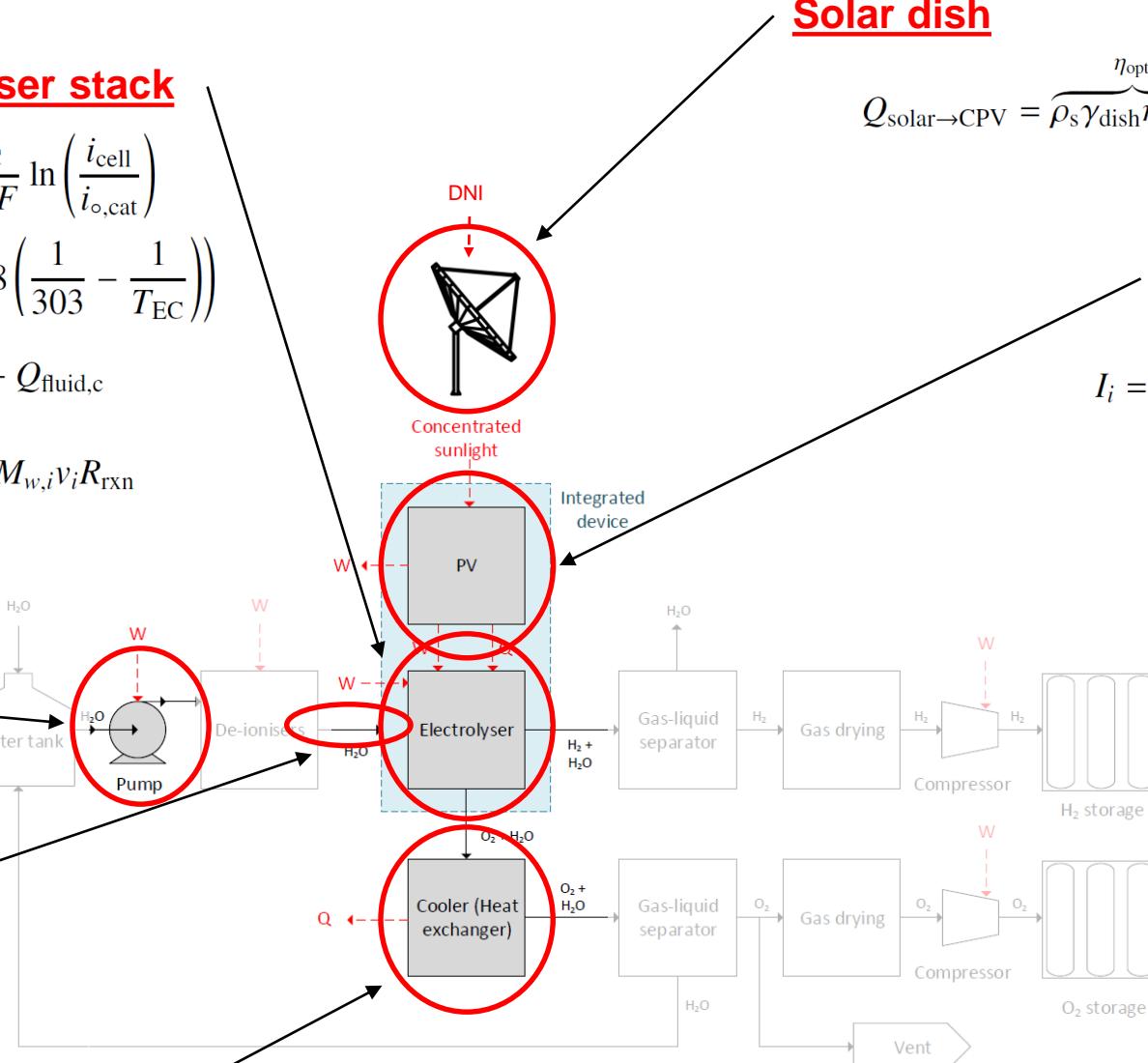
$$\Delta P = K_{\text{flow}} \left(\frac{Q_L}{N_{\text{EC,s}}} \right)^{\alpha_{\text{flow}}}$$

Pump

$$P_{\text{pump}} = \frac{\Delta P_{\text{sys}} F_{\text{pump}}}{\eta_{\text{pump}}}$$

Pipes

Heat exchanger



Solar dish

$$Q_{\text{solar} \rightarrow \text{CPV}} = \overbrace{\rho_s \gamma_{\text{dish}} \eta_{\text{clean}} A_{\text{dish}}}^{\eta_{\text{opt}}} \times \text{DNI}$$

CPV module

$$I_i = I_{\text{L},i} - I_{\text{o},i} \left[\exp\left(\frac{q(V_i + I_i R_{\text{s},i})}{n_i k_B T_{\text{PV}}}\right) - 1 \right] - \frac{V_i + I_i R_{\text{s},i}}{R_{\text{sh},i}}$$

$$0 = f_{\text{abs}} P_{\text{total}} - V_{\text{PV}} I_{\text{PV}} - Q_{\text{PV} \rightarrow \text{HS}}$$

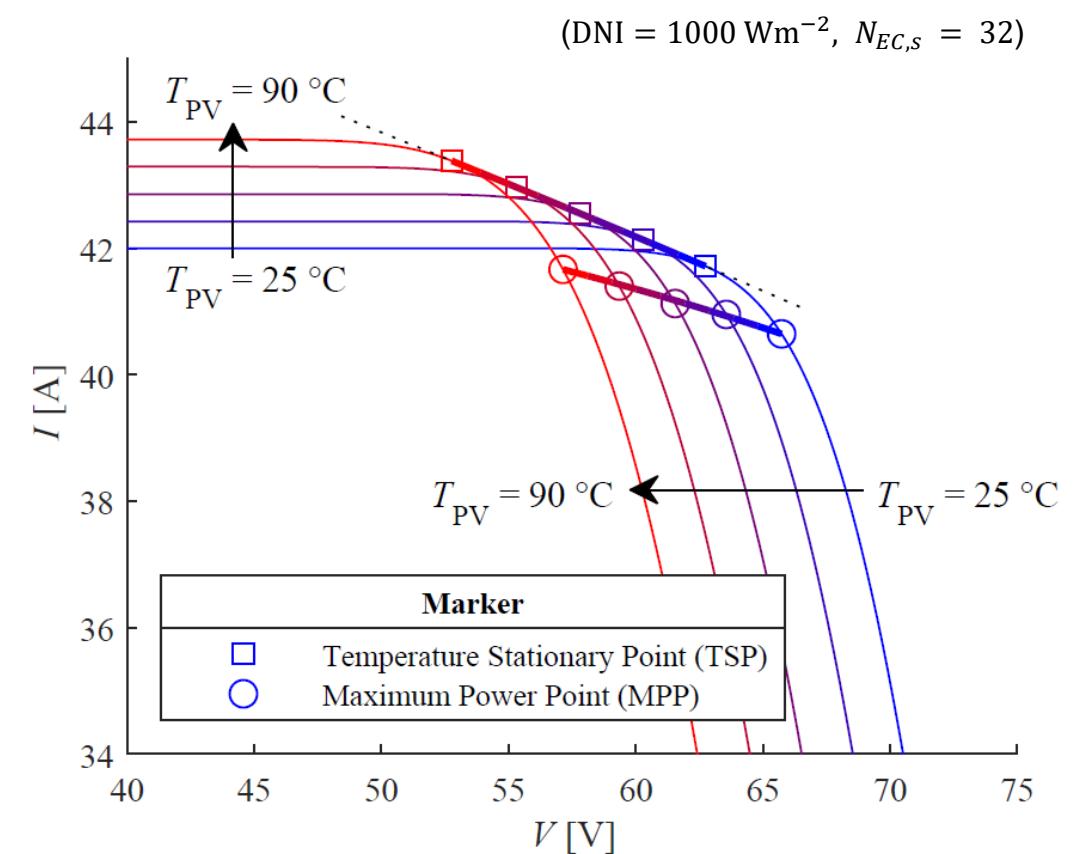
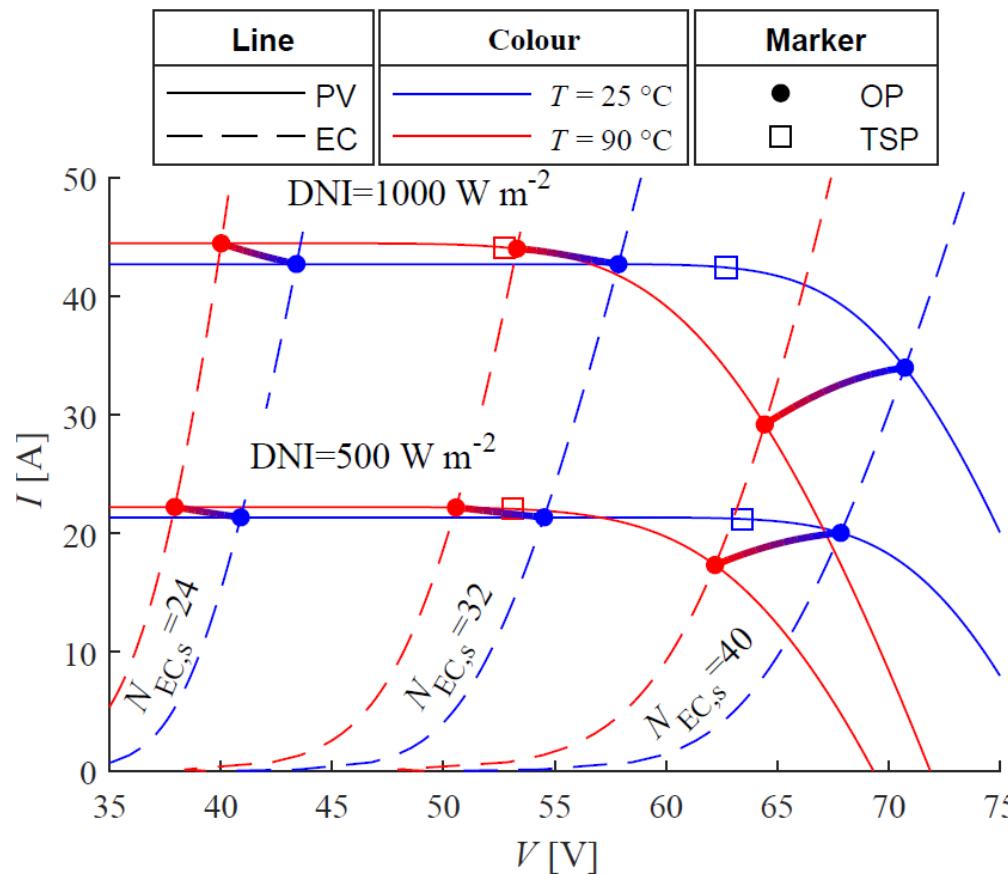
$$C_{\text{HS}} \frac{dT_{\text{HS}}}{dt} = Q_{\text{PV} \rightarrow \text{HS}} - Q_{\text{HS} \rightarrow \text{CW}} - Q_{\text{HS} \rightarrow \text{amb}}$$

$$\text{NTU} = \frac{\eta_o U_{\text{HS} \rightarrow \text{CW}} A_{\text{HS}}}{c_{p,\text{CW}} \dot{m}_{\text{CW}}}$$

$$\Delta P = f_D \frac{L \rho v^2}{2 D_h}$$

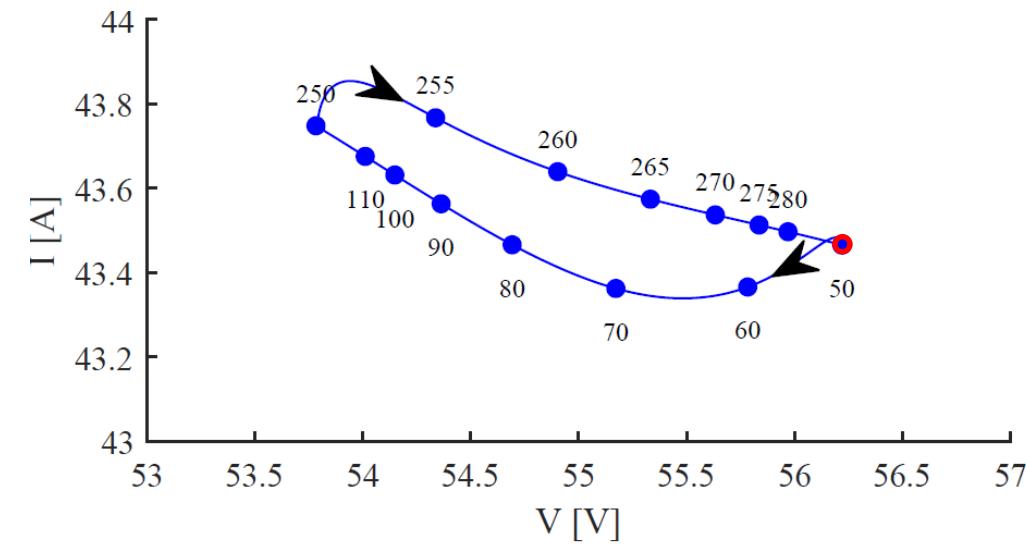
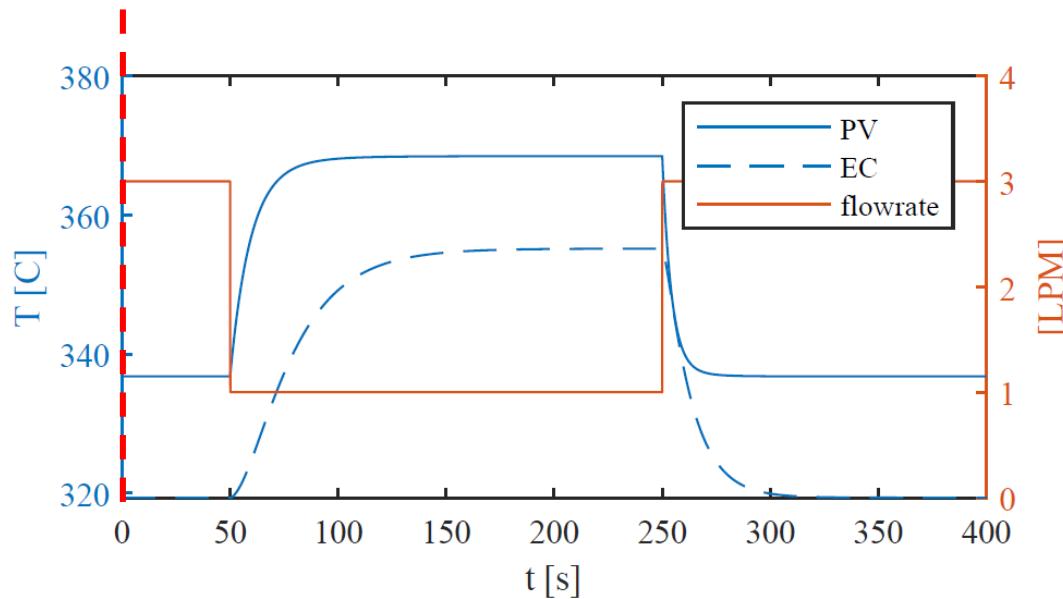
Temperature Dependence of Electrical Models

- Position of operating point heavily dependent on operating temperature (here shown for isothermal case)
- Behavior dependent on position of operating point relative to what we define as the “Temperature Stable Point” of the PV: $\left(\frac{dI_{PV}}{dT_{PV}} = 0\right)$

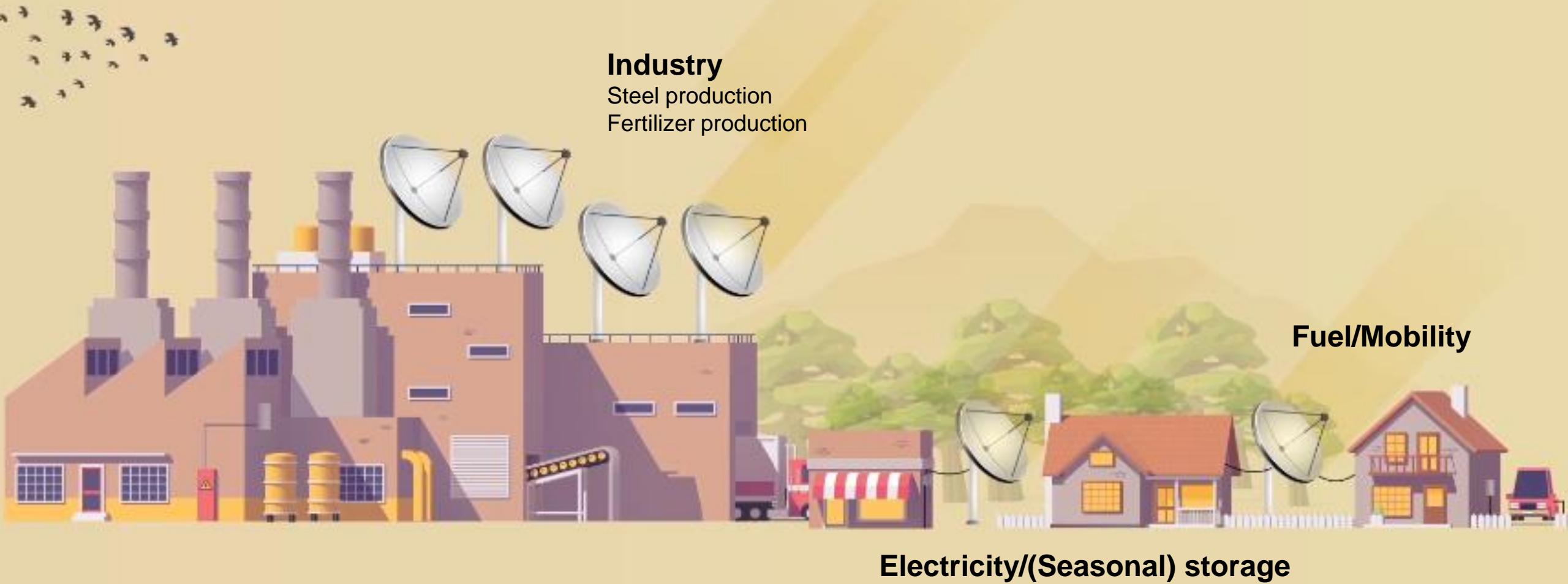


System Dynamics to Step Changes

- Dynamics in the electrical performance of the CPV and the EC originates from the changes in their operating temperatures
- Leads to non-linear behaviour – operating point hysteresis
- Step change in flowrate ($3 \rightarrow 1 \text{ L min}^{-1}$):

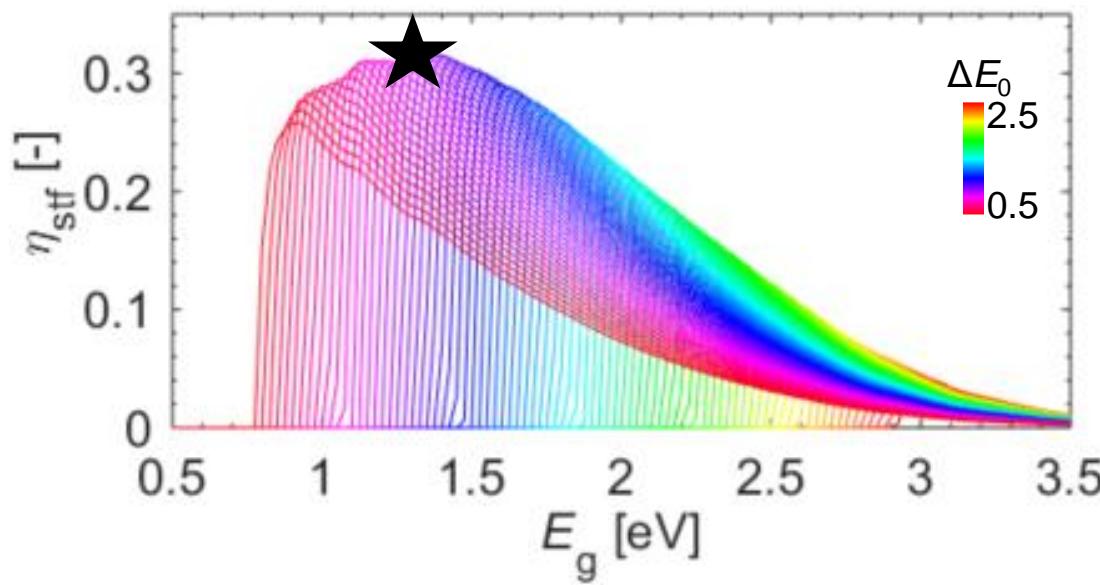


<http://www.sohhytec.com>

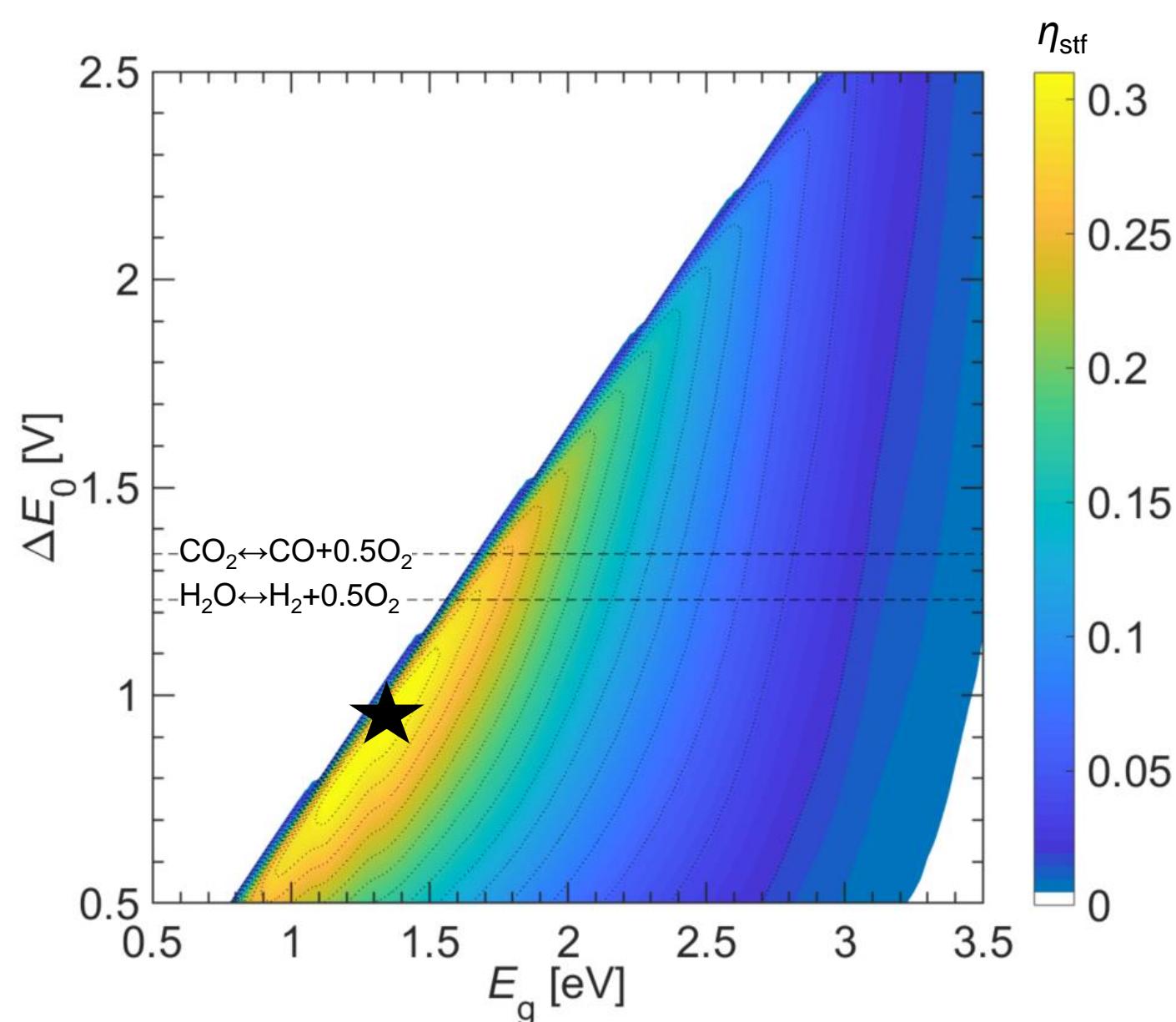


Beyond water splitting

- Which reactions are interesting?
- Limiting efficiencies:



Global maxima:
 $\eta_{\text{STF}} = 32\%$ at $E_g = 1.35$ eV and $\Delta E_0 = 0.96$ V



Acknowledgements



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